

SCANNING OPTICAL APPARATUS AND IMAGE FORMING  
APPARATUS USING THE SAME

BACKGROUND OF THE INVENTION

5 Field of the Invention

The present invention relates to a scanning optical device and an image forming apparatus using the same. In particular, the present invention relates to a scanning optical device suitable for an  
10 image forming apparatus such as a laser beam printer, a digital copying machine, or a multifunction printer, which has, for example, an electrophotographic process, in which a light flux emitted from light source means is deflected on an optical deflector  
15 (polygon mirror) serving as a deflection element and then a surface to be scanned is scanned with the light flux through a scanning optical element having an f $\theta$  characteristic to thereby record image information.

20 Related Background Art

Up to now, in a scanning optical device used for a laser beam printer (LBP) or the like, image recording is conducted through the following process. A light flux which is modulated according to an image  
25 signal in light source means and emitted therefrom is periodically deflected on, for example, an optical deflector composed of a rotating polygonal mirror

(polygon mirror). Then, the deflected light flux is converged in a spot shape onto a photosensitive recording medium (photosensitive drum) by a scanning optical element having an  $f\theta$  characteristic, to  
5 thereby scan the surface of the recording medium is scanned with the light flux.

Fig. 8 is a schematic view showing a main part of a conventional scanning optical device. In Fig. 8, a divergent light flux emitted from light source  
10 means 91 is converted into a substantially parallel light flux by a collimator lens 92. The substantially parallel light flux (the amount of light) is limited by an aperture stop 93 and incident into a cylindrical lens 94 having refractive power  
15 only in the sub scanning direction. Of the substantially parallel light flux incident into the cylindrical lens 94, a light flux within the main scanning section exits from the cylindrical lens 94 without being changed in its optical state; a light  
20 flux within the sub scanning section is converged and imaged as a substantially linear image near a deflection surface 95a of an optical deflector 95 composed of a rotating polygonal mirror (polygon mirror).

25 The light flux which is reflected and deflected on the reflection surface 95a of the optical deflector 95 is guided onto a photosensitive drum

surface 97 serving as a surface to be scanned through a scanning optical element (scanning lens system) 96 having an  $f\theta$  characteristic while the optical deflector 95 is rotated in a direction indicated by an arrow A. Accordingly, the photosensitive drum surface 97 is scanned with the light flux in a direction indicated by an arrow B (main scanning direction) to thereby record image information.

At this time, a part of the light flux (BD light flux), which is reflected and deflected on the optical deflector 95, is returned using a synchronous detection mirror (BD mirror) 81 through the scanning lens system 96 and incident into synchronous detection unit 84. The synchronous detection unit 84 includes: a slit (BD slit) 82 serving as synchronous position determining means which is located at a position optically equivalent to the photosensitive drum surface 97; and a synchronous detection element (BD sensor) 83. A timing of a writing start position (scanning start position) on the photosensitive drum surface 97 in the main scanning direction is adjusted based on a synchronous signal obtained from the synchronous detection unit 84. Therefore, a scanning line is produced on the photosensitive drum surface 97 to conduct image recording.

In recent years, with a tendency of size reduction of the main body of the image forming

apparatus, a compact optical system is required for the scanning optical device. In particular, the synchronous detection optical system (BD optical system) that adjusts the timing of the scanning start position is desired to be more compact because of a limitation on leading of electric wirings from the BD sensor and a limitation on arrangements in a casing (optical box).

In general, the BD optical system uses a portion (end) of the scanning lens, images a part of the light flux (BD light flux) deflected on the optical deflector at a position where the BD sensor is disposed or in the vicinity thereof to adjust the timing of the scanning start position.

An example in which a size of such BD optical system is reduced is disclosed in, for example, Japanese Patent No. 3254367. Japanese Patent No. 3254367 discloses an optical system in which the synchronous detection optical element (BD lens) is composed of an independent anamorphic lens and the BD lens is disposed at a position further apart from the optical deflector than the scanning lens.

The optical system according to Japanese Patent No. 3254367 is effective in reducing a size of the BD optical system and a cost thereof. However, because the BD lens is disposed at a position farther apart from the optical deflector than the scanning lens,

the distance between the BD lens and the BD sensor becomes shorter. Thus, there is a problem in that the synchronous detection cannot be conducted with high precision.

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#### SUMMARY OF THE INVENTION

An object of the present invention is to provide a scanning optical device having a compact and simple structure, in which the coupling  
10 efficiency of a collimator lens can be improved without reducing the precision of synchronous detection of a scanning start position on a surface to be scanned, and to provide an image forming apparatus using the scanning optical device.

15 A scanning optical apparatus according to the present invention includes:

light source means;

a first optical element that inputs a light flux emitted from the light source means to output  
20 the light flux;

a second optical element that converts the light flux emitted from the first optical element into a longitudinal linear image in a main scanning direction;

25 a deflection element that deflects the light flux emitted from the second optical element for scanning;

a third optical element that guides the light flux deflected by the deflection element to a surface to be scanned;

a synchronous detection element that obtains a  
5 synchronous signal; and

a fourth optical element that guides the light flux deflected by the deflection element to the synchronous detection element,

in which the second optical element and the  
10 fourth optical element are independent of each other, and

in a case where a point at which a main light beam traveling toward a scanning center on the surface to be scanned is deflected by the deflection  
15 element is assumed as a reference point, the second optical element is located at a position which is farther from the reference point than the fourth optical element.

## 20 BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a main scanning sectional view showing Embodiment 1 of the present invention;

Fig. 2 is a sub scanning sectional view showing Embodiment 1 of the present invention;

25 Fig. 3 is a main scanning sectional view showing Embodiment 2 of the present invention;

Fig. 4 is a sub scanning sectional diagram

showing an image forming apparatus according to an embodiment of the present invention;

Fig. 5 is a main scanning sectional view showing Embodiment 3 of the present invention;

5 Fig. 6 is a sub scanning sectional view showing Embodiment 3 of the present invention;

Fig. 7 is a sub scanning sectional diagram showing a color image forming apparatus according to an embodiment of the present invention; and

10 Fig. 8 is a schematic view of a main part of a conventional scanning optical device.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

(Embodiment 1)

15 Fig. 1 is a main part sectional view showing a scanning optical device in a main scanning direction, according to Embodiment 1 of the present invention (main scanning sectional view). Fig. 2 is a main part sectional view showing the scanning optical  
20 device of Fig. 1 in a sub scanning direction (sub scanning sectional view).

Here, the main scanning direction indicates a direction perpendicular to the rotational axis of a deflection unit and the optical axis of a scanning  
25 optical unit (direction of a light flux which is reflected and deflected (which is deflected for scanning) by the deflection unit). A sub scanning

direction indicates a direction parallel to the rotational axis of the deflection unit. In addition, a main scanning section indicates a plane which is parallel to the main scanning direction and includes  
5 the optical axis of a scanning optical unit. A sub scanning section indicates a plane perpendicular to the main scanning section.

In Figs. 1 and 2, light source means 1 is composed of, for example, a semiconductor laser. A  
10 condenser lens (collimator lens) 2 serving as a first optical element converts a divergent light flux emitted from the light source means 1 into a substantially parallel light flux (or substantially convergent light flux). An aperture stop 3 limits a  
15 passing light flux to shape it into a beam form. An optical system (cylindrical lens) 4 serving as a second optical element has predetermined power in only the sub scanning direction. By means of the optical system 4, the light flux passing through the  
20 aperture stop 3 is formed into a substantially linear image on a deflection surface (reflection surface) 5a of an optical deflector 5 (described later) within the sub scanning section. Note that elements such as the collimator lens 2, the aperture stop 3, and the  
25 cylindrical lens 4 compose an element of an incident optical system.

The optical deflector 5 serving as the



deflection element is composed of, for example, a polygon mirror having four surfaces (rotating polygonal mirror) and rotated in a direction indicated by an arrow "A" in Fig. 1 at a constant speed by a drive unit such as a motor (not shown).

A scanning lens system (scanning optical system) 6 serving as a third optical element has a condensing function and an  $f\theta$  characteristic and is composed of a first toric lens 61 and a second toric lens 62, each of which is made of a plastic material. The first toric lens 61 has refractive power mainly in the main scanning direction. The first toric lens 61 is disposed near the optical deflector 5, contributing to composing a compact scanning optical device. The second toric lens 62 has refractive power mainly in the sub scanning direction. The second toric lens 62 is disposed sufficiently apart from the optical deflector 5, reducing manufacturing sensitivity of the lens. The first toric lens 61 and the second toric lens 62 have refractive powers different from each other in the main scanning direction and the sub scanning direction, respectively. In addition, the first toric lens 61 and the second toric lens 62 have a tangent error correcting function in the case where a light flux related to image information, which is reflected and deflected on the optical deflector 5, is imaged onto

a photosensitive drum surface 8 serving as a surface to be scanned, and a conjugate relationship is made between the deflection surface 5a of the optical deflector 5 and the photosensitive drum surface 8 within the sub scanning section.

Reference numeral 65 denotes a protection-against-dust glass.

A synchronous detection optical element serving as a fourth optical element (hereinafter indicated as "BD lens") 73 is composed of an anamorphic lens which has different refractive powers within the main scanning section and the sub scanning section and is made of a plastic material. By means of the synchronous detection optical lens, a light flux (BD light flux) is imaged at a position where a synchronous detection element 72 (described later) is disposed or in the vicinity thereof, within the main scanning section. In addition, the BD lens 73 is disposed in a region between an optical path from the light source means 1 to the optical deflector 5 and an optical path from the optical deflector 5 to the surface to be scanned 8.

A synchronous detection unit 7 includes a synchronous detection slit 71 (hereinafter indicated as "BD slit") and an optical sensor serving as the synchronous detection element (hereinafter indicated as "BD sensor") 72. The BD slit 71 is disposed at a

position optically equivalent to the photosensitive drum surface 8 and determines a write start position of an image. The synchronous detection unit 7 adjusts a timing of a scanning start position for  
5 image recording on the photosensitive drum surface 8 in the main scanning direction, based on a synchronous signal (BD signal) obtained by detecting an output signal from the BD sensor 72.

In this embodiment, the cylindrical lens 4 and  
10 the BD lens 73 are independent of each other. In the case where a point at which a main light beam traveling toward the scanning center on the surface to be scanned 8 is deflected on the optical deflector 5 is assumed as a reference point P, the cylindrical  
15 lens 4 is located at a position which is farther from the reference point P than the BD lens 73. In other words, a distance from the reference point P, which is a deflection point of a light flux traveling toward the scanning center on the optical deflector 5,  
20 to the cylindrical lens 4 is longer than a distance to the BD lens 73.

Note that the BD slit 71 is integrally formed with a holder member that holds the semiconductor laser 1. The BD sensor 72 and the semiconductor  
25 laser 1 are both disposed on an electrical board 51. In addition, elements such as the BD lens 73, the BD slit 71, and the BD sensor 72 compose an element of a

synchronous detection optical system (hereinafter indicated as "BD optical system").

In this embodiment, a light flux emitted from the semiconductor laser 1 is converted into a  
5 substantially parallel light flux by the collimator lens 2. The light flux (the amount of light) is limited by the aperture stop 3 and then incident into the cylindrical lens 4. Of the substantially parallel light flux incident into the cylindrical  
10 lens 4, a light flux within the main scanning section is exited without changing its optical state. A light flux within the sub scanning section is converged and imaged as a substantial linear image (linear image extended in the main scanning  
15 direction) onto the deflection surface 5a of the optical deflector 5. Then, the light flux which is reflected and deflected on the deflection surface 5a of the optical deflector 5 is imaged in a spot shape onto the photosensitive drum surface 8 through the  
20 first toric lens 61, the second toric lens 62, and the protection-against-dust glass 65. At this time, the optical deflector 5 is rotated in a direction indicated by an arrow "A", so that the photosensitive drum surface 8 is optically scanned in a direction  
25 indicated by an arrow "B" (main scanning direction) at a constant speed. Thus, image recording is conducted on the photosensitive drum surface 8

composing a recording medium.

At this time, in order to adjust the timing of the scanning start position on the photosensitive drum surface 8 before optical scanning is conducted on the photosensitive drum surface 8, a part of the light flux (BD light flux) which is reflected and deflected on the optical deflector 5 is condensed onto the surface of the BD slit 71 by the BD lens 73 and then guided to the BD sensor 72. Then, the timing of the scanning start position for image recording on the photosensitive drum surface 8 is adjusted based on the synchronous signal (BD signal) obtained by detecting an output signal from the BD sensor 72.

Hereinafter, an increase in precision of the synchronous detection and an improvement in coupling efficiency of the collimator lens will be described.

First, with respect to the increase in precision of the synchronous detection, the synchronous detection precision optically depends on a focal distance  $f_{BD}$  of the BD lens 73 within the main scanning section. This is because the focal distance  $f_{BD}$  of the BD lens 73 within the main scanning section becomes an angular velocity of a light flux on the BD sensor 72 (or BD slit). The optical synchronous detection precision improves as the focal distance value increases. However, in the case where the

focal distance is long, the BD optical system becomes larger, so that the entire device cannot be made compact.

Therefore, according to this embodiment, in the case where a focal distance of the scanning lens system 6 within the main scanning section is given as  $f_{f\theta}$  and the focal distance of the BD lens 73 within the main scanning section is given as  $f_{BD}$ , respective elements are set so as to satisfy a condition,

$$f_{f\theta}/3 < f_{BD} < f_{f\theta} \quad \dots(1).$$

Thus, it is possible to make the BD optical system compact while maintaining the increase in precision of the synchronous detection.

Next, with respect to the improvement in coupling efficiency of the collimator lens, in order to improve the coupling efficiency, it is necessary to set F numbers (F No.) of the collimator lens 2 in the main scanning direction and the sub scanning direction to be bright. In addition, there is a limit to the performance of F number of the collimator lens 2. Therefore, in order to maximize the coupling efficiency within limited brightness, it is desirable that the F number in the main scanning direction is made substantially equal to the F number in the sub scanning direction.

However, in many cases, in relation to the optical face tangle error correction, the F number of

the collimator lens 2 in the sub scanning direction is set to become darker than the F number thereof in the main scanning direction. In particular, in the case of a scanning lens system which has a smaller  
5 imaging magnification within the sub scanning section, such tendency is remarkable. Thus, low coupling efficiency is a problem.

Therefore, according to this embodiment, the F number in the sub scanning direction is set to be no  
10 larger than twice as much as the F number in the main scanning direction (a diameter of diaphragm Ds in the sub scanning direction is no smaller than 1/2 times a diameter of diaphragm Dm in the main scanning direction), thereby improving the coupling efficiency  
15 of the collimator lens 2.

In this embodiment, in the case where a spot shape on the surface to be scanned 8 is assumed to be substantially a circle and the F number is given by Fi, a diameter of diaphragm D disposed near the  
20 collimator lens 2 is as follows:

main scanning:  $D_m = f_{f\theta}/F_i$ ,

sub scanning :  $D_s = f_{c1} \times |\beta_{f\theta}|/F_i$ .

( $f_{c1}$ : focal distance of cylindrical lens within sub scanning section,

25  $\beta_{f\theta}$ : imaging magnification of scanning lens system within sub scanning section).

In order to set the diameter of diaphragm Ds in

the sub scanning direction to a value no smaller than 1/2 times the diameter of diaphragm  $D_m$  in the main scanning direction, it is necessary to satisfy conditions,

5            $D_m/2 < D_s,$   
             $f_{c1} > f_{f0}/(2|\beta_{f0}|) \quad \dots(2).$

Here, in order to achieve both the increase in precision of the synchronous detection and the improvement in coupling efficiency of the collimator  
10 lens 2, it is required that both the above-mentioned conditional expressions (1) and (2) are satisfied. That is, as is apparent from the above-mentioned conditional expressions, it is preferable to lengthen both the focal distance  $f_{BD}$  of the BD lens 73 within  
15 the main scanning section and the focal distance  $f_{c1}$  of the cylindrical lens 4 within the sub scanning section.

Therefore, in this embodiment, in order to compactly dispose an optical system while satisfying  
20 these conditions, the cylindrical lens 4 and the BD lens 73 each are composed of a separate optical element. In addition, assuming the deflection point P, at which a light flux traveling toward the scanning center is deflected on the optical deflector  
25 5, as a reference, the distance from the deflection point P to the cylindrical lens 4 is made longer than the distance to the BD lens 73.



Note that the distance from the deflection point P to the optical element (lens) indicates an optical path length measured along an actual optical path. In the case where a reflecting mirror is  
5 disposed on an optical path to deflect a light flux, the optical path is used for measuring the optical path length.

Parameter values of the respective elements in the scanning optical device according to this  
10 embodiment are as follows:

focal distance of scanning lens system within main scanning section  $f_{f\theta} = 150$ ;

imaging magnification of scanning lens system within sub scanning section  $|\beta_{f\theta}| = 1.38$ ;

15 focal distance of cylindrical lens within sub scanning section  $f_{c1} = 94.0$ ;

focal distance of BD lens within main scanning section  $f_{BD} = 76.4$ .

The above-mentioned parameter values satisfy  
20 the conditional expressions (1) and (2).

In this embodiment, the conditions

$$50 < f_{BD} < 150 \quad \dots (1),$$

$$f_{c1} > 54.4 \quad \dots (2)$$

may be satisfied. Both the focal distance  $f_{c1}$  of the  
25 cylindrical lens 4 within the sub scanning section and the focal distance  $f_{BD}$  of the BD lens 73 within the main scanning section satisfy these conditions.

As described above, according to this embodiment, the cylindrical lens 4 and the BD lens 73 each are composed of a separate optical element. In addition, assuming the deflection point P, at which the light flux traveling toward the scanning center is deflected on the optical deflector 5, as the reference, the distance from the deflection point P to the cylindrical lens 4 is made longer than the distance to the BD lens 73. Thus, the incident optical system and the BD optical system in which the increase in precision of the synchronous detection and the improvement in coupling efficiency of the collimator lens 2 are both achieved can be compactly and simply constructed.

Note that, the scanning lens system 6 is composed of two lenses in this embodiment. However, the present invention is not limited to this. The scanning lens system 6 may be composed of, for example, a single lens or three or more lenses. In addition, the BD sensor and the semiconductor laser are disposed on the same electrical board in this embodiment. However, the present invention is not limited to this. The BD sensor and the semiconductor laser may be disposed on different electrical boards.

(Embodiment 2)

Fig. 3 is a main part sectional view showing a scanning optical device in the main scanning

direction, according to Embodiment 2 of the present invention. In Fig. 3, the same reference numerals are provided to the same elements as shown in Fig. 1.

In this embodiment, points different from the  
5 above-mentioned Embodiment 1 are that: a multi-beam semiconductor laser is used as the light source means; a reflecting mirror 77 is disposed in an incident optical system and a BD optical system; and the focal distance of the cylindrical lens 4 and the  
10 focal distance of the BD lens 74 are changed accordingly. Other structures and optical actions are substantially the same as Embodiment 1, and the same effect is obtained.

In other words, in Fig. 1, light source means  
15 (multi-beam light source) 11 is composed of a separately modulatable multi-beam semiconductor laser. The reflecting mirror 77 changes an optical path and is disposed in the incident optical system and the BD optical system. A synchronous detection optical  
20 element 74 serving as a fourth optical element (BD lens) is composed of an anamorphic lens which has different refractive powers within the main scanning section and the sub scanning section and is made of a plastic material. By means of the synchronous  
25 detection optical lens, a light flux (BD light flux) is imaged at a position where the BD sensor 72 is disposed or at the vicinity thereof, within the main

scanning section.

In this embodiment, a plurality of light fluxes which are independently modulated by the multi-beam semiconductor laser 11 and exited therefrom are  
5 converted into substantially parallel light fluxes by the collimator lens 2. The substantially parallel light fluxes (the amount of light) is limited by the aperture stop 3 and then incident into the cylindrical lens 4. Of the light fluxes incident  
10 into the cylindrical lens 4, light fluxes within the main scanning section are exited without changing their optical state, reflected on the reflecting mirror 77, and incident into the deflection surface 5a of the optical deflector 5. Light fluxes within  
15 the sub scanning section are converged, reflected on the reflecting mirror 77, and imaged as a substantial linear image (linear image extended in the main scanning direction) onto the deflection surface 5a of the optical deflector 5. Then, the plurality of  
20 light fluxes which are reflected and deflected on the deflection surface 5a of the optical deflector 5 are imaged in spot shapes onto the photosensitive drum surface 8 through the first toric lens 61, the second toric lens 62, and the protection-against-dust glass  
25 65. At this time, the optical deflector 5 is rotated in the direction indicated by the arrow "A", so that the photosensitive drum surface 8 is optically

scanned in the direction indicated by the arrow "B"  
(main scanning direction) at a constant speed. Thus,  
image recording is conducted on the photosensitive  
drum surface 8 composing a recording medium.

5       At this time, in order to adjust the timing of  
the scanning start position on the photosensitive  
drum surface 8 before optical scanning is conducted  
on the photosensitive drum surface 8, a part of the  
light fluxes (BD light fluxes) which are reflected  
10 and deflected on the optical deflector 5 is condensed  
onto the surface of the BD slit 71 through the  
reflecting mirror 77 by the BD lens 74 and then  
guided to the BD sensor 72. Then, the timing of the  
scanning start position for image recording on the  
15 photosensitive drum surface 8 is adjusted based on  
the synchronous signal (BD signal) obtained by  
detecting an output signal from the BD sensor 72.

Note that, although not used in this embodiment,  
an additional optical element may be provided near  
20 the BD slit 71 to obtain a substantial conjugate  
relationship between the reflecting mirror 77 and the  
BD sensor 72 with respect to the sub scanning section.  
In the case where such an optical element is used, an  
irradiation position on the BD sensor 72, which is  
25 changed due to a tangle error of the reflecting  
mirror 77 can be corrected.

In this embodiment, the reflecting mirror 77 is

disposed on the optical path from the light source means 11 to the optical deflector 5 and on the optical path from the optical deflector 5 to the BD sensor 72. Accordingly, there is an advantage in that a long optical path length can be ensured while keeping the incident optical system and the BD optical system compact. In particular, in the case of the multi-beam scanning optical device, in order to detect the synchronization of the plurality of light fluxes by the single BD sensor 72, it is necessary to sufficiently separate the light fluxes from one another on the BD sensor 72 in the main scanning direction. Thus, it is required that the focal distance of the BD lens 74 within the main scanning section is further lengthened.

Parameter values of the respective elements in the scanning optical device according to this embodiment are as follows:

focal distance of scanning lens system within main scanning section  $f_{f\theta} = 150$ ;

imaging magnification of scanning lens system within sub scanning section  $|\beta_{f\theta}| = 1.38$ ;

focal distance of cylindrical lens within sub scanning section  $f_{c1} = 114$ ;

focal distance of BD lens within main scanning section  $f_{BD} = 96$ .

The above-mentioned parameter values satisfy

the conditional expressions (1) and (2).

In this embodiment, the conditions

$$50 < f_{BD} < 150 \quad \dots(1),$$

$$f_{c1} > 54.4 \quad \dots(2)$$

5 may be satisfied. Both the focal distance  $f_{c1}$  of the cylindrical lens 4 within the sub scanning section and the focal distance  $f_{BD}$  of the BD lens 74 within the main scanning section satisfy these conditions.

Also, in this embodiment, a relationship  
10 expression,

$$f_{c1} \times |\beta_{f\theta}| \equiv f_{f\theta}$$

is established. In other words, because a diameter of diaphragm on the surface to be scanned 8 becomes substantially a circle and thus the F number in the  
15 main scanning direction becomes equal to the F number in the sub scanning direction. Therefore, the coupling efficiency of the collimator lens 2 can be further improved.

As described above, according to this  
20 embodiment, as in the above-mentioned Embodiment 1, the cylindrical lens 4 and the BD lens 74 each are composed of a separate optical element. In addition, assuming the deflection point P, at which the light flux traveling toward the scanning center is  
25 deflected on the optical deflector 5, as the reference, the distance from the deflection point P to the cylindrical lens 4 is made longer than the

distance to the BD lens 74. Thus, the incident optical system and the BD optical system in which the increase in precision of the synchronous detection and the improvement in coupling efficiency of the collimator lens 2 are both achieved can be compactly and simply constructed.

Further, with respect to the feature inherent in this embodiment, the reflecting mirror 77 is disposed on the optical path from the light source means 11 to the optical deflector 5 and on the optical path from the optical deflector 5 to the BD sensor 72. Therefore, a long optical path length can be ensured while keeping the incident optical system and the BD optical system compact. Therefore, the plurality of light fluxes are easily separated from one another on the BD sensor 72 and the coupling efficiency of the collimator lens 2 can be further improved.

#### Image Forming Apparatus

Fig. 4 is a main part sectional view showing an image forming apparatus in the sub scanning direction, according to an embodiment of the present invention. In Fig. 4, reference numeral 104 denotes an image forming apparatus. Code data Dc is inputted from an external device 117 such as a personal computer to the image forming apparatus 104. The code data Dc is converted into image data (dot data) Di by a printer



controller 111 in the image forming apparatus 104.  
The image data Di is inputted to an optical scanning  
unit 100 having the structure indicated in  
Embodiments 1 and 2. A light beam 103 modulated  
5 according to the image data Di is emitted from the  
optical scanning unit 100, and the photosensitive  
surface of a photosensitive drum 101 is scanned with  
the light beam 103 in the main scanning direction.

The photosensitive drum 101 serving as an  
10 electrostatic latent image bearing member  
(photosensitive member) is rotated clockwise by a  
motor 115. According to the rotation, the  
photosensitive surface of the photosensitive drum 101  
is moved in the sub scanning direction orthogonal to  
15 the main scanning direction with respect to the light  
beam 103. A charging roller 102 for uniformly  
charging the surface of the photosensitive drum 101  
is provided above the photosensitive drum 101 so as  
to be contact with the surface thereof. The surface  
20 of the photosensitive drum 101, which is charged by  
the charging roller 102, is irradiated with the light  
beam 103 for scanning by the optical scanning unit  
100.

As described earlier, the light beam 103 is  
25 modulated according to the image data Di. The  
surface of the photosensitive drum 101 is irradiated  
with the light beam 103 to form an electrostatic

latent image thereon. The electrostatic latent image is developed as a toner image by a developing unit 107 provided in the downstream side from the irradiation position of the light beam 103 in the rotational direction of the photosensitive drum 101 so as to be contact with the photosensitive drum 101.

The toner image developed by the developing unit 107 is transferred onto a sheet 112 serving as a material to be transferred by a transfer roller 108 provided below the photosensitive drum 101 so as to oppose to the photosensitive drum 101. The sheet 112 is contained in a sheet cassette 109 located in the front (right side in Fig. 4) of the photosensitive drum 101. Manual feed is also possible. A feed roller 110 is provided in the end portion of the sheet cassette 109. The sheet 112 in the sheet cassette 109 is sent to a transport path.

By the above operation, the sheet 112 to which an unfixed toner image is transferred is further transported to a fixing device located in the rear (left side in Fig. 4) of the photosensitive drum 101. The fixing device is composed of a fixing roller 113 having a fixing heater (not shown) therein and a pressure roller 114 provided to press the fixing roller 113. The sheet 112 transported from the transferring part is heated while it is pressurized by the press-contacting part between the fixing

roller 113 and the pressure roller 114, so that the unfixed toner image on the sheet 112 is fixed.

Further, a delivery roller 116 is provided in the rear of the fixing roller 113, and the sheet 112 with  
5 the fixed toner image is delivered to the outside of the image forming apparatus.

Although not shown in Fig. 4, the printer controller 111 conducts not only data conversion described earlier but also control of each part of  
10 the image forming apparatus, which is represented by the motor 115, control of a polygon motor in an optical scanning unit as described later, and the like.

(Embodiment 3)

15 Fig. 5 is a main part sectional view showing a scanning optical device in the main scanning direction, according to Embodiment 3 of the present invention (main scanning sectional view). Fig. 6 is a main part sectional view showing the scanning  
20 optical device of Fig. 5 in the sub scanning direction (sub scanning sectional view). In Figs. 5 and 6, the same reference numerals are provided to the same elements as shown in Fig. 1.

In this embodiment, points different from the  
25 above-mentioned Embodiment 1 are that: the present invention is applied to a tandem type scanning optical device in which a plurality of surfaces to be

scanned 8a to 8d are simultaneously scanned with light fluxes emitted from a plurality of light source means 1a to 1d; and the tandem type scanning optical device is mounted on a color image forming apparatus.

- 5 Other structures and optical actions are substantially the same as Embodiment 1, and the same effect is obtained.

In other words, in Figs. 5 and 6, SK1 denotes a first scanner and SK2 denotes a second scanner. The  
10 first scanner SK1 includes: light source means (1a, 1b); collimator lenses (2a, 2b) that convert a plurality of light fluxes emitted from the light source means (1a, 1b) into substantially parallel light fluxes; aperture stops (3a, 3b) that regulate  
15 the plurality of light fluxes from the collimator lenses (2a, 2b); cylindrical lenses (4a, 4b) that image the plurality of light fluxes as linear images extended in the main scanning direction; the single optical deflector 5 serving as a deflection element;  
20 and scanning lens systems (SLa, SLb) that form the plurality of light fluxes which are reflected and deflected on the optical deflector 5 in spot shapes on corresponding photosensitive drum surfaces (8a, 8b) serving as surfaces to be scanned. The second  
25 scanner SK2 includes: light source means (1c, 1d); collimator lenses (2c, 2d) that convert a plurality of light fluxes emitted from the light source means

(1c, 1d) into substantially parallel light fluxes; aperture stops (3c, 3d) that regulate the plurality of light fluxes from the collimator lenses (2c, 2d); cylindrical lenses (4c, 4d) that image the plurality  
5 of light fluxes as linear images extended in the main scanning direction; the single optical deflector 5 serving as a deflection element; and scanning lens systems (SLc, SLd) that form the plurality of light fluxes which are reflected and deflected on the  
10 optical deflector 5 in spot shapes on corresponding photosensitive drum surfaces (8c, 8d) serving as surfaces to be scanned.

The scanning lens systems (SLa, SLb, SLc, SLd) each have two toric lenses, i.e., first and second  
15 toric lenses (63ab, 64a, 64b; 63cd, 64c, 64d), each of which is made of a plastic material. According to the scanning lens systems, the plurality of light fluxes which are reflected and deflected on the optical deflector 5 are imaged in spot shapes onto  
20 the corresponding photosensitive drum surfaces (8a, 8b, 8c, 8d). In addition, the scanning lens systems (SLa, SLb, SLc, SLd) each have a tangle error correcting function in the case where a conjugate relationship is made between the vicinity of the  
25 reflection surface 5a of the optical deflector 5 and the vicinity of the photosensitive drum surfaces (8a, 8b, 8c, 8d) within the sub scanning section.

A synchronous detection optical lens serving as a fourth optical element (BD lens) 75 is composed of an anamorphic lens which has different refractive powers within the main scanning section and the sub scanning section and is made of a plastic material. By means of the synchronous detection optical lens, a light flux (BD light flux) is imaged at the position where a synchronous detection element 72 is disposed or in the vicinity thereof, within the main scanning section.

In this embodiment, the same optical deflector 5 is commonly used for the first scanner SK1 and the second scanner SK2. In addition, a light flux which is reflected and deflected on a different deflection surface of the optical deflector 5 is used for each of the first scanner SK1 and the second scanner SK2.

In this embodiment, a plurality of light fluxes emitted from the plurality of light source means (semiconductor lasers) 1a to 1d are converted into substantially parallel light fluxes by the collimator lenses 2a to 2d. The light fluxes (the amount of light) are limited by the aperture stops 3a to 3d and then incident into the cylindrical lenses 4a to 4d. Of the substantially parallel light fluxes incident into the cylindrical lens 4a to 4d, light fluxes within the main scanning section exits without being changed in its optical state. Light fluxes within

the sub scanning section are converged and imaged as substantial linear images (linear images extended in the main scanning direction) onto the deflection surfaces of the optical deflector 5. Then, the plurality of light fluxes which are reflected and deflected on the deflection surfaces of the optical deflector 5 are imaged in spot shapes onto the photosensitive drum surfaces 8a to 8d through the scanning lens systems (SLa, SLb, SLc, SLd) and protection-against-dust glasses 65a to 65d. At this time, the optical deflector 5 is rotated in a direction indicated by an arrow A, so that the photosensitive drum surfaces 8a to 8d are optically scanned in a direction indicated by an arrow B (main scanning direction) at a constant speed. Consequently, image recording is conducted on the photosensitive drum surfaces 8a to 8d composing recording mediums.

At this time, in order to adjust the timing of the scanning start position on the photosensitive drum surfaces 8a to 8d before optical scanning is conducted on the photosensitive drum surfaces 8a to 8d, a part of the light fluxes (BD light fluxes) which are reflected and deflected on the optical deflector 5 is condensed onto the surface of the BD slit 71 by the BD lens 75 and then guided to the BD sensor 72. Then, the timing of the scanning start

position for image recording on each of the photosensitive drum surfaces 8a to 8d is adjusted based on the synchronous signal (BD signal) obtained by detecting an output signal from the BD sensor 72.

5           Note that, in this embodiment, the single optical deflector is used and applied to a tandem type scanning optical device in which a part of toric lenses (scanning optical elements) is commonly used for a plurality of light fluxes. However, the  
10 present invention is not limited to this. For example, the present invention can be achieved for all tandem type scanning optical devices regardless of the number of optical elements such as optical deflectors, toric lenses, or cylindrical lenses, and  
15 there is no limitation on the number of optical elements.

Also, in this embodiment, the synchronous detection is conducted using only the single BD light flux and the other BD light fluxes are controlled  
20 based on the synchronous signal obtained from signal data of the other BD light fluxes in consideration of a divisional error and the like. The number of BD light fluxes for direct synchronous detection may be increased to two or more and the present invention is  
25 not limited to the number of BD light fluxes.

Parameter values of the respective elements in the scanning optical device according to this



embodiment are as follows:

focal distance of scanning lens system within  
main scanning section  $f_{f\theta} = 150$ ;

imaging magnification of scanning lens system  
5 within sub scanning section  $|\beta_{f\theta}| = 1.38$ ;

focal distance of cylindrical lens within sub  
scanning section  $f_{c1} = 96$ ;

focal distance of BD lens within main scanning  
section  $f_{BD} = 76.4$ .

10 The above-mentioned parameter values satisfy  
the conditional expressions (1) and (2).

In this embodiment, the conditions

$$50 < f_{BD} < 150 \quad \dots(1),$$

$$f_{c1} > 54.4 \quad \dots(2)$$

15 may be satisfied. Both the focal distance  $f_{c1}$  of the  
cylindrical lens 4 within the sub scanning section  
and the focal distance  $f_{BD}$  of the BD lens 73 within  
the main scanning section satisfy these conditions.

According to this embodiment, in order to  
20 compactly dispose an optical system while satisfying  
these conditions, the cylindrical lens 4 and the BD  
lens 75 each are composed of a separate optical  
element. In addition, in the case where the  
deflection point P at which the light flux traveling  
25 toward the scanning center is deflected on the  
optical deflector 5 is assumed as the reference, the  
distance to the cylindrical lens 4 becomes longer

than the distance to the BD lens 75. Thus, the incident optical system and the BD optical system can be compactly and simply constructed, the systems attaining higher precision in the synchronous  
5 detection while attaining improvement in the coupling efficiency of the collimator lens 2.

#### Color Image Forming Apparatus

Fig. 7 is a main part schematic diagram showing a color image forming apparatus according to an  
10 embodiment of the present invention. This embodiment shows a tandem type color image forming apparatus that irradiates the surface of a photosensitive drum serving as an image bearing member with four light fluxes from a scanning optical device to record image  
15 information. In Fig. 7, reference numeral 260 denotes a color image forming apparatus; 210, a scanning optical device having the structure described in Embodiment 3; 221, 222, 223 and 224, respective photosensitive drums serving as image  
20 bearing members; and 231, 232, 233, and 234, respective developing units.

In Fig. 7, respective color signals of R (red), G (green), and B (blue) are inputted from an external device 270 such as a personal computer to the color  
25 image forming apparatus 260. The color signals are converted into respective image data (dot data) of C (cyan), M (magenta), Y (yellow), and B (black) by a

printer controller 271 in the color image forming apparatus 260. These image data are inputted to the scanning optical device 210. Light beams 103 modulated according to the respective image data are  
5 emitted from the scanning optical device 210. The photosensitive surfaces of the photosensitive drums 221, 222, 223 and 224 are scanned with the light beams in the main scanning direction.

According to the color image forming apparatus  
10 in this embodiment, as described above, latent images of the respective colors are formed on the corresponding surfaces of the photosensitive drums 221, 222, 223 and 224 using four light fluxes which correspond to respective color light fluxes from the  
15 scanning optical device and are based on image data. After that, multi-transfer is conducted on a recording material to produce a full color image.

For example, a color image reading apparatus including a CCD sensor may be used as the external  
20 device 270. In this case, the color image reading apparatus and the color image forming apparatus 260 compose a color digital copying machine.

As described above, according to this embodiment, as in Embodiment 1, the cylindrical lens  
25 and the BD lens each are composed of a separate optical element. In addition, in the case where the deflection point P at which the light flux traveling

toward the scanning center is deflected on the optical deflector 5 is assumed as the reference, it is constructed such that the distance to the cylindrical lens becomes longer than the distance to the BD lens. Thus, the incident optical system and the BD optical system can be compactly and simply constructed, the systems attaining higher precision in the synchronous detection while attaining improvement in the coupling efficiency of the collimator lens.

Further, with respect to the feature inherent in this embodiment, the present invention is applied to the tandem type scanning optical device and the color image forming apparatus. Thus, even in the case of a tandem type scanning optical device in which the number of parts is large and the degree of freedom in arrangements is small, the synchronous detection can be easily conducted in compact arrangements.

According to the present invention, as described above, the cylindrical lens and the synchronous detection optical element each are composed of a separate optical element. In addition, in the case where the point at which a main light beam traveling toward the scanning center on the surface to be scanned is deflected on the deflection element is assumed as the reference point, the

cylindrical lens is located at a position which is farther from the reference point than the synchronous detection optical element. Thus, there can be achieved a scanning optical device in which the  
5 incident optical system and the synchronous detection optical system can be compactly and simply constructed, the systems attaining higher precision in the synchronous detection while attaining improvement in the coupling efficiency of the  
10 collimator lens. In addition, an image forming apparatus using the scanning optical device can be achieved.